

Optimization of Double Pipe Heat Exchanger with Response Surface Methodology Using Nanofluid and Twisted Tape

Farhad Fadakar Kourkah¹, Dariush Khosravi Mahd¹, Mojtaba Mirzaee^{2,*}

¹Department of Mechanical Engineering, Sciences Faculty, Saveh Branch, Islamic Azad University, Saveh, Iran

²Young Researchers and Elite Club, Omidiyeh Branch, Islamic Azad University, Omidiyeh, Iran

Email address:

mo.mirzaee2020@gmail.com (M. Mirzaee)

*Corresponding author

To cite this article:

Farhad Fadakar Kourkah, Dariush Khosravi Mahd, Mojtaba Mirzaee. Optimization of Double Pipe Heat Exchanger with Response Surface Methodology Using Nanofluid and Twisted Tape. *Fluid Mechanics*. Vol. 3, No. 3, 2017, pp. 20-28. doi: 10.11648/j.fm.20170303.12

Received: April 30, 2017; **Accepted:** May 25, 2017; **Published:** June 30, 2017

Abstract: The performance of a double pipe heat exchanger is analyzed using Response Surface Methodology (RSM) with various input parameters namely Reynolds number, twisted ratio(y/w) and concentration of SiO₂ nanofluid of the output response the overall heat transfer coefficients of the double pipe heat exchanger. The experimental design is developed based on Box - Behnken design method. The influence of vital input parameters and interaction among them are investigated using analysis of variance (ANOVA). optimum value of the overall heat transfer coefficients is 2732.59(w/m².k) when the Reynolds number ut is 19999.42, concentration(0.5%w) and twisted ratio(y/w) 5.87. In the desirability function approach, the value of desirability was 0.937 for the RSM model very close to The predicted RSM model is found to be capable of predictive overall heat transfer coefficients of double pipe heat exchanger.

Keywords: Double Pipe Heat Exchanger, SiO₂ Nanofluid, Central Composite Design

1. Introduction

The convective heat transfer can be enhanced passively by changing the flow geometry, boundary conditions, or by enhancing the thermal conductivity of the fluid. Researchers tried to increase the heat transfer rate by increasing the thermal conductivity of the fluid. As a new research and technology frontier, Nano fluids are used to enhance heat transfer. Nano fluids are engineered colloids which are made of a base fluid and nanoparticles (1-100) nm. The advantages of Nano fluids are: (1) higher thermal conductivity than that predicted by currently available macroscopic models, (2) excellent stability, and (3) little penalty due to an enhancement in pressure drop and pipe wall erosion experienced by suspensions of micrometer or millimeter particles [1]. Such advantages of Nano fluid offer important benefits for numerous applications in many fields such as petrochemical, refining, electronic, transportation, medicine, heating, and air- conditioning. Another alternative method to enhance heat transfer is to insert twisted tape into a core tube. This approach induces secondary

recirculation to the axial flow, leading to an increase in tangential and radial turbulent fluctuation and thus reducing a thickness of the boundary layer.

Albadr [2] et al. experimental study on the forced convective heat transfer and flow characteristics of a Nano fluid consisting of water and different volume concentrations of Al₂O₃ Nano fluid (0.3–2)% flowing in a horizontal shell and tube heat exchanger counter flow under turbulent flow conditions are investigated. The Al₂O₃ nanoparticles of about 30 nm diameter are used in the present study.

Madhesh et al [3], experimental investigate carried heat transfer potential and rheological characteristics of copper and titanium hybrid Nano fluids using a tube in the counter flow heat exchanger. The Nano fluids were prepared by dispersing the surface functionalized and crystalline copper and titanium hybrid Nano composite in the base fluid.

Keshavarz Moraveji et al [4], CFD modeling of laminar forced convection on Al₂O₃ Nano fluid with size particles equal to 33 nm and particle concentrations of 0.5, 1 and 6 wt.% Three-dimensional steady-state governing partial differential equations was discretized using finite volume method.

Influences of some important parameters such as nanoparticle concentration and Reynolds number on the enhancement of nano fluid heat transfer have been investigated.

Ahmed [5] et al. laminar forced convection flow of Al_2O_3 -water Nano fluid in sinusoidal-wavy channel is numerically studied. The two-dimensional governing equations of continuity, momentum and energy equations in body-fitted coordinates are solved using finite volume method.

Azmi [6] et al. Nano fluids systems only used for increase the heat transfer. The enhancement in heat transfer coefficients in combination with structural modifications of flow systems namely, the addition of tape inserts. Experiments are undertaken to determine heat transfer coefficients and friction factor of TiO_2 /water Nano fluid up to 0.3% volume concentration at an average temperature of 30 C.

Celen et al [7] investigation numerical model having two-dimensional equations was obtained by a CFD program and experimental data were evaluated for the verification procedure of the numerical data outputs. Hydrodynamics and thermal behaviors of the water- TiO_2 flow were calculated by constant heat flux and temperature-dependent settings.

Sekhara Reddy et al [8] investigated heat transfer, friction factor and thermal performance of three Nano fluids different blends were prepared with ethylene glycol and water and TiO_2 nanoparticles and characterized for thermal conductivity as a function of temperature and volume concentration of nanoparticles. Based on the experimental results, it is observed that the thermal conductivity of TiO_2 nano fluids.

Using nano fluid together with twisted taped for heat transfer enhancement was reported in numerous research

works such as twisted tape inserts with Al_2O_3 /water nanofluid [9] and [10], helical twist tape inserts with Al_2O_3 /water nano fluid [11], twisted tape with alternate axis inserts with CuO /water nano fluid [12], twisted tape inserts with CuO /water nano fluid in corrugated tube [13], dual twisted tape inserts with CuO /water nanofluid in micro-fin tube [14], helical screw tape inserts with Al_2O_3 /water nano fluids [15], helical screw tape inserts using CuO /water nanofluids [16], and propeller inserts with TiO_2 /water nano fluid [17].

Moreover, Nagarajan et al. [18] reported that the geometries of left-right twisted tapes played an important role in governing heat transfer, friction factor and thermal performance.

In the present study will apply the quadratic model of RSM associated the Box-Behnken design (BBD) with four factors and three levels in order to establish an effective optimal procedure for optimizing the design parameters of double pipe heat exchanger with inner twisted tape tube. The corresponding mathematical models were developed by regressive analysis and then tested by analysis of variance (ANOVA) to examine the accuracy.

2. Experimental

2.1. Twisted Tapes

In the test run, tapes are used with three different twist ratios $y = 6, 4.3$ and 2.5 . Twisted tapes are made from stainless steel strips of thickness 0.9 mm and width 8 mm as shown in figure 2. To produce the modified twisted tape, the typical twists changed by changing twist ratio and geometrical progression ratio along the twist.

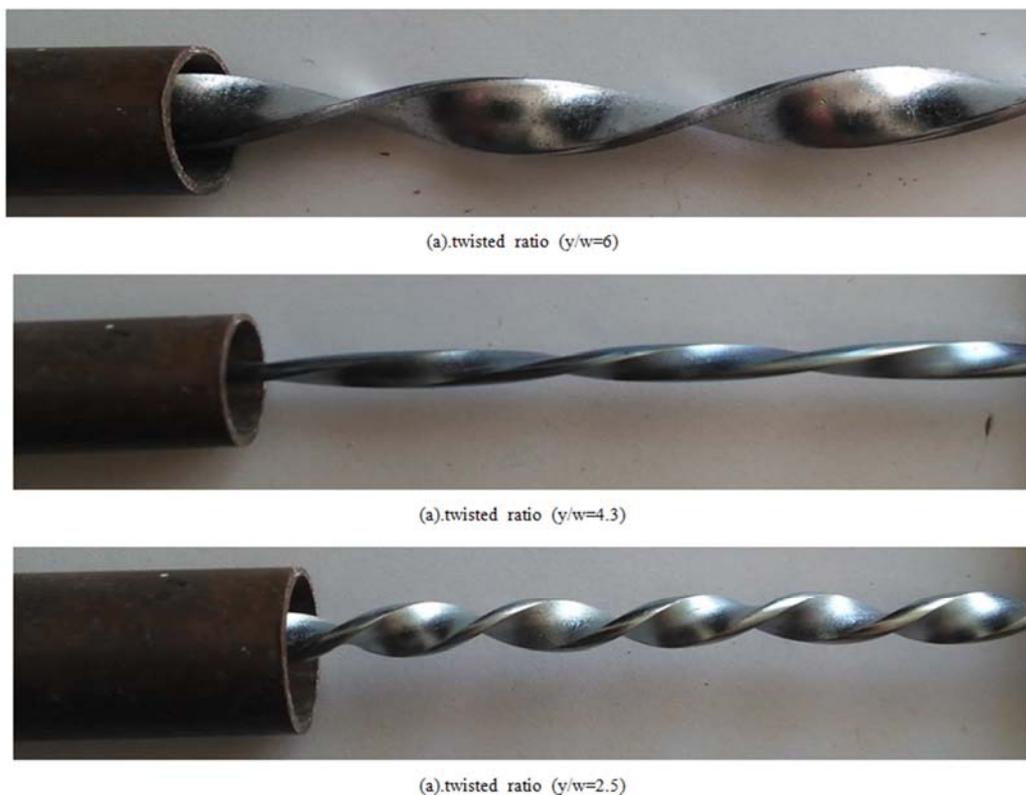


Figure 1. Schematic of tested Twisted Tapes inserts, (a). twisted ratio ($y/w=6$), (b). twisted ratio ($y/w=4.3$), (c). twisted ratio ($y/w=2.5$).

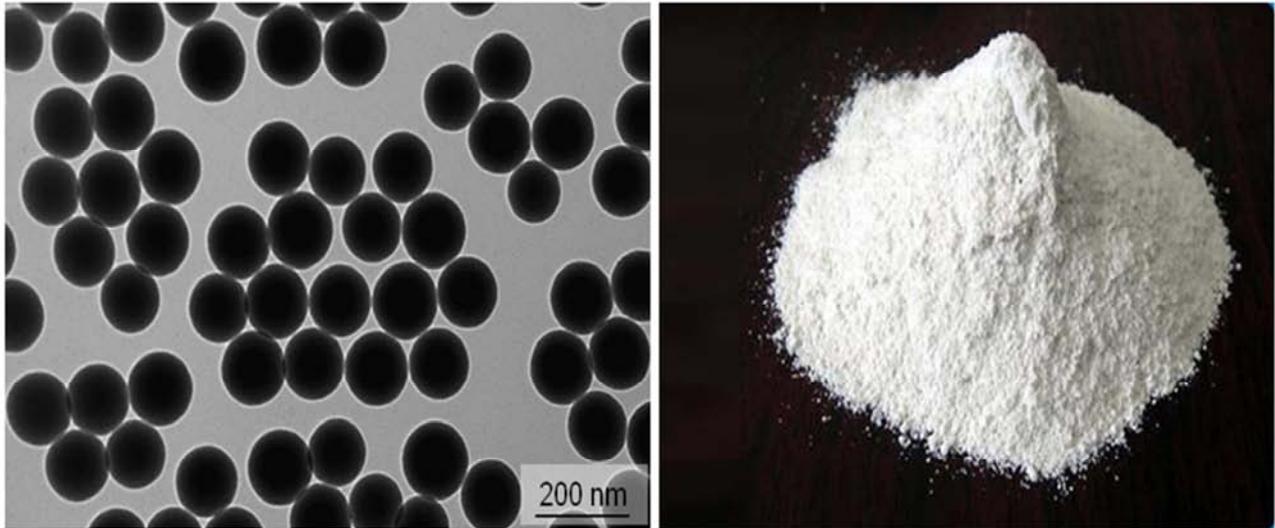


Figure 2. SEM image of SiO₂ nanoparticles.

2.2. Preparation of Materials Nanofluid

The nanoparticles of SiO₂ nanoparticles of size 15-20 nm purchased in zigma rich, Bangalore, india. The nano particles are used at the ratio of 0.1-0.5% with distilled water. A ChromTech sonicator (Taiwan) with 40 kHz and 1200W with variable intensities was used to ensure that the nanoparticles were well dispersed in the water. The nanoparticles are weighed to the required ratio and then mixed with base fluid and then allowed for sonication to get the entire particles for soluble in the distilled water. The sonication is done for 2-3 hours continuously. The properties of SiO₂ nanoparticles is shown in table 1.

Table 1. SiO₂ nanoparticles properties.

Property	SiO ₂ nanoparticles
Appearance	White powder
Diameter	15-20 nm
Surface area	640m ² /gr
Density	2.4gr/cm ³
Purity	99.50%

$$\% \text{Mass concentration} = \frac{w_{np}}{w_{bf} + w_{np}} \tag{1}$$

where

w_{np} = amount of nanoparticles in gram
 w_{bf} = amount of base fluid(water) in gram

Figure 2 shows SEM images of the SiO₂ and it was found that SiO₂ nanoparticles shows nearly spherical morphology.

The experimental investigation of heat transfer characteristic of Nano fluid was carried out using the experimental apparatus as shown in figure 3. It mainly consists of a test section, receiving tanks in which working fluids are stored, heating and cooling system, thermometer, flow meter, Rota-meter, pressure measurement system and data acquisition system. The working fluids were circulated through the loop by using variable speed pumps of suitable capacity. The test section is of 1.2 m length with counter

flow path within horizontal double pipe heat exchanger in which hot Nano fluid was applied inside the tube while cooling water was directed through the annulus. The inside pipe is made of a soft steel tube with the inner diameter of 9mm, outer diameter of 0.011m and thickness of 0.002m while the outside pipe is of steel tube with the inner diameter of 16mm, outer diameter of 0.018m and thickness of 2mm. The twisted tapes were made from aluminum sheet with tape thickness (d) of 0.001m, and width (W) of 0.005m and length of 1.2m. The tape thickness of 0.001m was chosen to avoid an additional friction in the system that might be occurred by the thicker tape. To measure the inlet and outlet temperature of the Nano fluid and cold water at the inlet and outlet of the test section, 4 thermocouples of type J were used. All of the thermocouples were calibrated before fixing them. All four evaluated temperature probes were connected to the data logger sets. An electric heater and a thermostat installed on it were used to maintain the temperature of the Nano fluid. During the test, the mass flow rate and the inlet and outlet temperatures of the Nano fluid and cold water were measured. To measure the pressure drop across the test section, differential pressure transmitter was mounted at the pressure tab located at the inlet and outlet of the section. The Nano fluid flow rate was measured by a magnetic flow meter which was placed at the entrance of the test section. For each test run, it was essential to record the data of the temperature, volumetric flow rates and pressure drop across the section at steady state conditions. Two storage tanks made of stainless steel at capacity of 15 lit were used to collect the fluids leaving the test section. Hot nano fluid was pumped from the fluid tank through the inner tube included twisted tapes at different Reynolds number between 2000 to 20000. To ensure the steady state condition for each run, the period of around 15-20 minutes depending on Reynolds number and twisted tapes was taken prior to the data record. After initial experiment without twisted tape, the insert was placed inside the tube. Similarly, all the steps were repeated keeping the twisted tape at stationary position and the data were recorded.

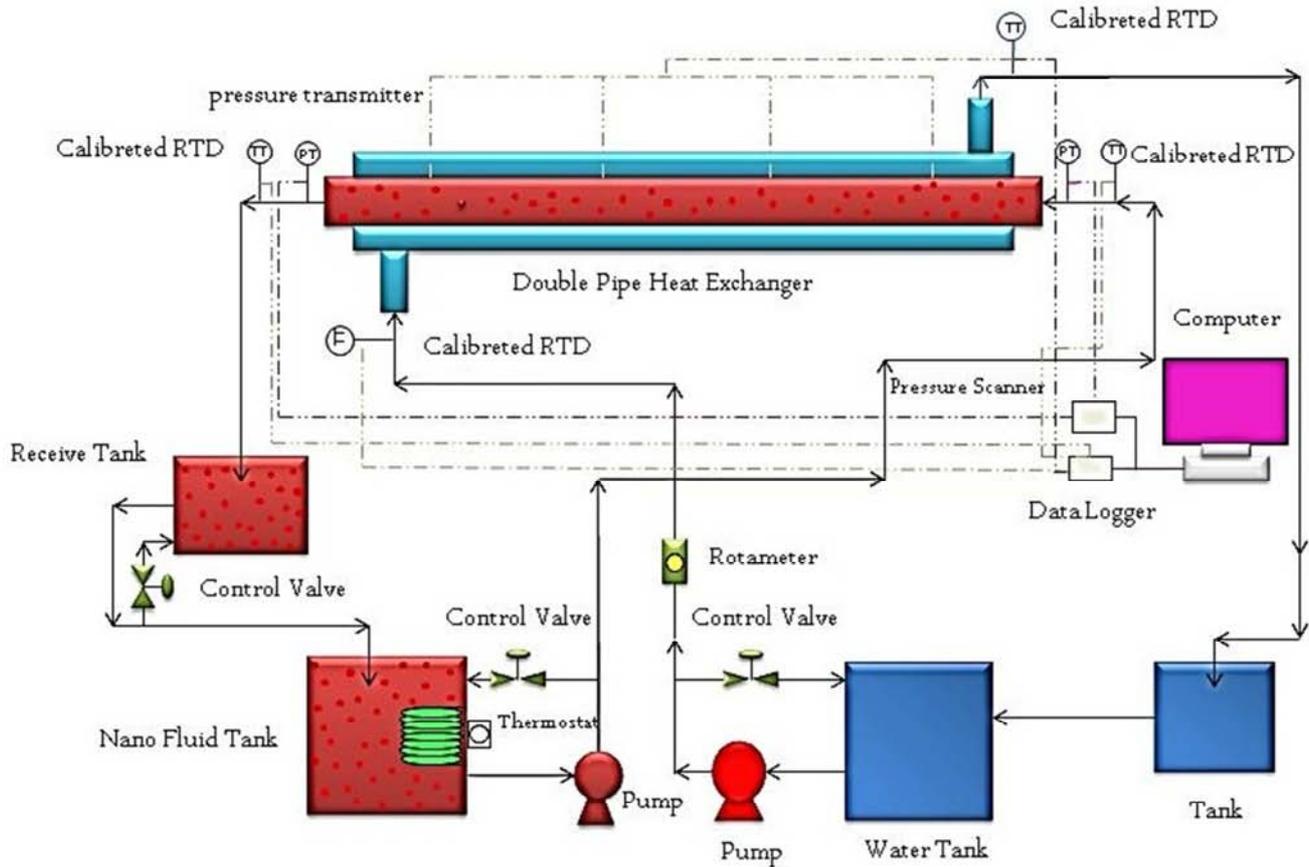


Figure 3. Schematic of experimental setup.

The uncertainties calculated with the maximum possible error for the parameters and various instruments is given in Table 2.

Table 2. Uncertainty of experimental parameters in heat transfer with double pipe heat exchanger.

parameters	Uncertainty
Mass flow nanofluid	±0.28
Mass flow water	±0.35
T _{wall}	±0.15
T _{bulk}	±0.101
Δp	±0.19
Overall heat transfer	6.23-17.50%
Q (hot nanofluid)	8.31-15.69%
Q (cold fluid)	6.23-17.58%

3. Response Surface Methodology

It is a combined mathematical and statistical technique based on the fit of a polynomial equation (empirical models) to the experimental data. This method generates a polynomial function for response relating it to the variables involved. In doing so it deals with the variables only at specific levels (mostly -1, 0, 1). RSM generates an experimental design for model preparation. An experimental design is a specific set of experiments defined by a matrix composed of the different

level combinations of the variables studied. Different methods of determining the response surface require a different experimental design. Generally, the relationship between the response and the independent variables is unknown. The most common forms are low-order polynomials (first or second-order). The simplest model which can be used in RSM is based on a linear function:

$$Y = \beta_0 + \sum_{i=1}^k \beta_i x_i + \epsilon \tag{2}$$

where k is the number of variables, β₀ is the constant term, β_i represents the coefficients of the linear parameters, x_i represents the variables, and ε is the residual associated to the experiments.

The next level of the polynomial model should contain additional terms, which describe the interaction between the different experimental variables. This way, a model for a second-order interaction presents the following terms:

$$Y = \beta_0 + \sum_{i=1}^k \beta_i x_i + \sum_{i=1}^k \beta_{ii} x_i^2 + \epsilon \tag{3}$$

In order to determine a critical point (maximum, minimum, or saddle), it is necessary for the polynomial function to contain quadratic terms according to the equation presented below:

$$Y = \beta_0 + \sum_{i=1}^k \beta_i x_i + \sum_{i=1}^k \beta_{ii} x_i^2 + \sum_{1 \leq i < j}^k \beta_{ij} x_i x_j + \epsilon \tag{4}$$

Where, β_{ij} represents the coefficients of the quadratic parameter. A second-order model can significantly improve the optimization process when a first order model suffers lack of fit due to interaction between variables.

The mathematical model found after fitting the function to the data can sometimes not satisfactorily describe the experimental domain studied. So, the quality of the model fitted is evaluated by the application of analysis of variance (ANOVA). RSM regressively fits the experimental readings of the design to a model (first, second or higher order) and determines the coefficients involved (β). General designs corresponding to these models are: i. First-Order Designs: The most common first-order designs are 2k factorial (k is the number of control variables), Plackett–Burman, etc. ii. Second-Order Designs: The most frequently used second-order designs are the 3 k factorial, central composite, and the Box–Behnken designs, etc.

The application of three-level factorial designs is not frequent, and the use of this design has been limited to the optimization of two variables because its efficiency is very low for higher numbers of variables. The central composite design is still the symmetrical second order experimental design most utilized for the development of analytical procedures. The Box–Behnken design present more efficient matrices and is more economical and hence has increased

number of published works in recent years. That is, Box–Behnken design requires least number of experimental runs and hence is most economical and most suitable in case where less no. of experimental runs is performed.

Box–Behnken design

- (1) Requires an experiment number according to $N=2k(k-1) + cp$, where k is the number of factors and (cp) is the number of the central points.
- (2) ii. All factor levels have to be adjusted only at three levels (-1, 0, +1) with equally spaced intervals between these levels

4. Results and Discussion

In this experimental study the performance of the double pipe heat exchanger is analyzed by response surface methodology (RSM). Box Behnken design method is employed with 3 input parameters namely Reynolds number (A), concentration (w%) (B) and twisted ratio(y/w) (C) over the output response as overall heat transfer. DESIGN-EXPERT software is used for this analysis. Table 3 shows the range of input parameters. In RSM -1 means the minimum and +1 denotes the maximum value of each input parameters.

Table 3. Actual and Coded values for different parameters involved.

Factor	Name	Type	Low Actual	High Actual	Low Coded	High Coded	Mean
A	Re	Numeric	2000	20000	-1	1	11000
B	Con (w%)	Numeric	0.2	0.5	-1	1	0.35
C	twisted ratio (y/w)	Numeric	2.5	6	-1	1	4.25

Table 4. ANOVA for Response Surface Quadratic Model – overall heat transfer coefficients.

Source	Sum of Squares	df	Mean Square	F Value	p-value, Prob > F	
Model	1.37E+06	9	1.52E+05	30.46	0.0008	significant
A-Re	1.14E+06	1	1.14E+06	228.47	< 0.0001	
B-con(w%)	56907.57	1	56907.57	11.41	0.0197	
C-twisted ratio(y/w)	62018.9	1	62018.9	12.43	0.0168	
AB	14981.76	1	14981.76	3	0.0336	
AC	155.38	1	155.38	0.031	0.8668	
BC	18483.76	1	18483.76	3.71	0.0122	
A^2	13264.63	1	13264.63	2.66	0.0039	
B^2	472.93	1	472.93	0.095	0.0406	
C^2	63557.32	1	63557.32	12.74	0.0161	
Residual	24940.88	5	4988.18			
Lack of Fit	23328.84	3	7776.28	9.65	0.0954	not significant
Pure Error	1612.04	2	806.02			
Cor Total	1.39E+06	14				
R-Squared	0.9821					
Adj R-Squared	0.9498					
Pred R-Squared	0.7293					
Adeq Precision	17.382					

The computed values of the overall heat transfer coefficients are entered in the software design matrix. The Box–Behnken response surface methodology is used to

develop the relationship between the experimental variables and the response that is overall heat transfer coefficients. A regression analysis is carried out to

develop a best fit of the model to the experimental data, which are used to generate response surface plots. Table 4 shows the analysis of variance (ANOVA). The values of “Prob>F” less than 0.05 indicates model terms are significant. The value 0.05 shows that the regression is statistically significant at a 95% confidence level ($P < 0.05$). For the present case Reynolds number (A), twisted ratio(y/w) (C) are playing significant effect than the concentration (w%) (B). The square values of Reynolds number (A), twisted ratio(y/w) (C) and concentration (w%) (B) are also having significant effect on the performance of the double pipe heat exchanger. The interaction effect between Reynolds number and concentration (w%) (AB) also has significant effect. The interaction effect of concentration (w%) with twisted ratio(y/w) (BC) also made some significant effect on the efficiency. The other effect like AC is insignificant.

The “Pred R-Squared” value of 0.9821 (coefficient of determination) is in responsible agreement with “Adj R-Squared” of 0.9498. Adequate precision measures the signal to noise ratio. Here the ratio of 17.382 indicates an adequate signal. This model can be used to navigate the design space. The model F value is 30.46 and a probability value is less than 0.001 which indicates that the model is significant for to finding the overall heat transfer coefficients of the double pipe heat exchanger. The sum of squares due to lack of fit, or more tersely a lack-of-fit sum of squares, is one of the components of a partition of the sum of squares in an analysis of variance, used in the numerator in an F-test.

Based on ANNOVA, different coefficients were estimated to develop the following empirical relation to predict the overall heat transfer coefficients of the double pipe heat exchanger. The values are Prob > F less than the 0.05 indicates that the terms are significant and values are greater than the 0.1 indicates that the insignificants. The lack of fit F value is 9.65 means the lack of fit not significant and it relative to the pure error. Non significant of lack of fit is good for model to fit. Based on the ANNOVA, the following empirical relation was developed to predict the overall heat transfer coefficients of the double pipe heat exchanger. The df denotes the degree of freedom of the model and that value is 9. It is the number of values in the final calculation of a statistic that are free to vary. Mean squares are used in analysis of variance and are calculated as a sum of squares divided by its appropriate degrees of freedom.

$$\text{Overall heat transfer} = 1463.68732 + 0.075765(\text{Re}) - 391.74643\text{con}(\text{w}\%) + 227.55027\text{twisted ratio}(\text{y/w}) - 0.045333(\text{Re})\text{con}(\text{w}\%) - 3.95714\text{E}-004(\text{Re})\text{twisted ratio}(\text{y/w}) + 258.96190\text{con}(\text{w}\%)^2 - 42.84082\text{twisted ratio}(\text{y/w})^2 \quad (5)$$

The working fluid in this analysis is SiO₂ nanofluid. The base fluid used in the SiO₂ nanofluid is DI water. The equation 5 valid for the experiments within the range of double pipe heat exchanger operation mentioned in the table 3.

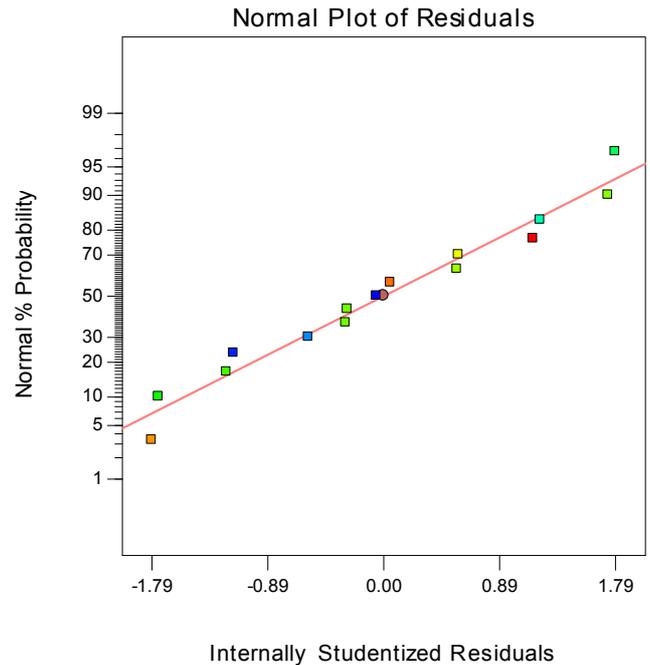


Figure 4. Normal plot of residual on overall heat transfer coefficients.

Figure 4 shows the normal plot of residuals for overall heat transfer coefficients of the double pipe heat exchanger, which indicates that errors in the experiments are normally distributed.

It is observed from Figures 5-7 that the overall heat transfer coefficients of double pipe heat exchanger increases linearly with an increase the Reynolds number in the test section. In general, the increase of nanofluid concentration results in the following consequences: (1) the increases of thermal conductivity and collision of nanoparticles which are favorite factors for heat transfer enhancement and (2) an increase of fluid viscosity which diminishes the fluid movement and thus heat transfer rate. The obtained result implies that for the present range, the effect of the increase in thermal conductivity and the collision of nanoparticles are more prominent than the increase of the fluid viscosity. It is evident from Figures 6 and 7 that when a twisted tape is inserted into a plain tube there is a significant improvement in overall heat transfer coefficients because of secondary flow, with greater enhancement being realized at higher Reynolds numbers and lower twist ratios.

From the figure 7 it is evident that the overall heat transfer coefficients increases with the decrease twisted ratio. The overall heat transfer coefficients of the double pipe heat exchanger reaches a maximum at twisted ratio(y/w=4.25) afterwards the overall heat transfer coefficients tends to decrease. This enhancement is mainly due to the centrifugal forces resulting from the spiral motion of the fluid and partly due to the tape acting as fin. It is observed that the reduction in tape width causes reduction in overall heat transfer coefficients as well as reduction in pressure drop.

One reason for this difference in heat transfer at high Reynolds numbers is the high viscosity of nanofluid. In general, the fluid containing rod-shaped particles, due to

severe reactions, has high viscosity and high density in shear flow. Particle concentration and movement of particles in the flow are other factors that affect the heat transfer [6]. The transitional move is assumed the main mechanism for increasing the thermal conductivity of nanoparticles. The mobility of finer particles increases the coefficient of thermal conductivity of nanofluids more than the coarse particles. Twisted-tape inserts increase the heat transfer coefficients with relatively small increase in the pressure drop [3-4].

The thickness of the thermal boundary layer decides the amount of the diffusion heat transfer from wall to fluid. At lower twist ratio, the thickness of thermal boundary layer is small, causing a very small amount of diffusion heat transfer. Therefore, the overall heat transfer is mainly because of the convective currents generated by the transverse velocity. They are known to be one of the earliest swirl flow devices employed in the single phase heat transfer processes. Because of the design and application convenience they have been widely used over decades to generate the swirl flow in the fluid. Size of the new heat exchanger can be reduced significantly by using twisted tapes in the new heat exchanger for a specified heat load [8]. Thus, it provides an economic advantage over the fixed cost of the equipment. Twisted tapes can be also used for retrofitting purpose. They

can increase the heat duties of the existing double tube heat exchangers [8]. Twisted tapes with multitube bundles are easy to fit and remove and thus enable tube side cleaning in fouling situations. Inserts such as twisted tape, wire coils, ribs, and dimples mainly obstruct the flow and separate the primary flow from the secondary flows. This causes the enhancement of the heat transfer in the tube flow. Inserts reduce the effective flow area thereby increasing the flow velocity. A complete uncertainty analysis was also made to estimate the errors associated with experiments. The overall heat transfer occurring from tube to fluid is due to combined effect of conduction and convection. Tube flow can be divided into two parts- boundary flow and core flow. The boundary flow is a fluid region near the wall, beyond which, in the tube, the core flow is defined. If the secondary flow created due to flow conditions (Twist ratio and Reynolds number) disturbs only the core flow, it will promote uniform temperature in core region and thus will enhance conduction heat transfer from wall to fluid. On the contrary if secondary flow disturbs boundary flow, convection heat transfer will dominate [7-9]. Thus it is important to analyze velocity profile and temperature profile near wall and at core to understand effect of secondary flow on heat transfer at various flow conditions [16-17].

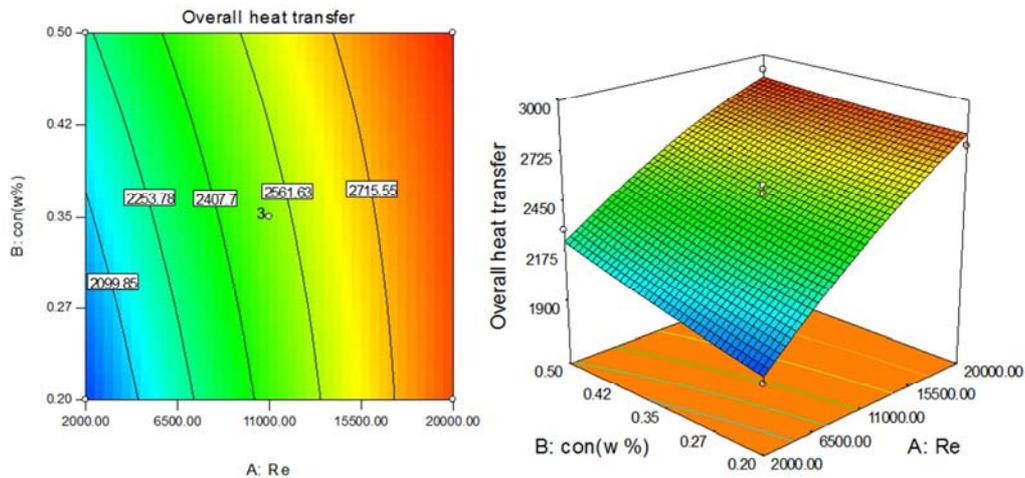


Figure 5. Response surface plots for the effect of the Reynolds number and the concentration on the overall heat transfer coefficients.

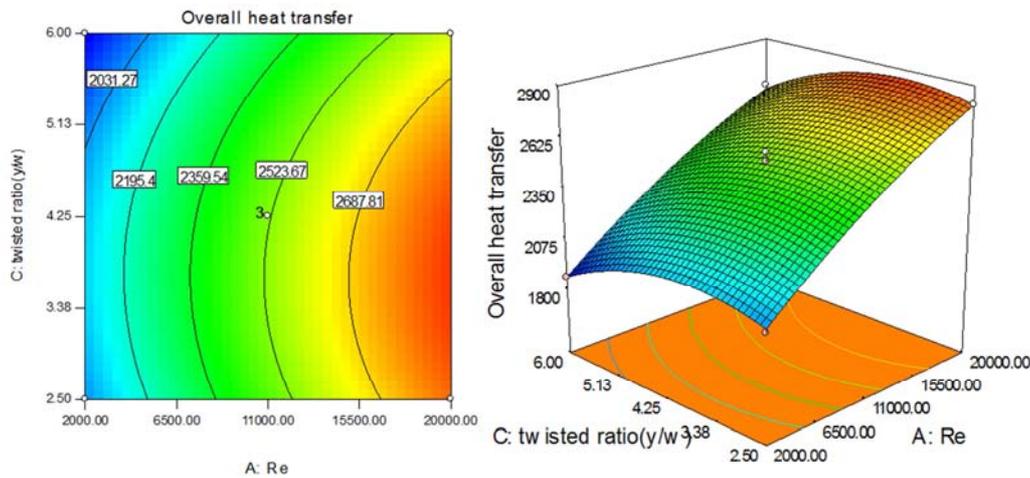


Figure 6. Response surface plots for the effect of the Reynolds number and twisted ratio(y/w) on the overall heat transfer coefficients.

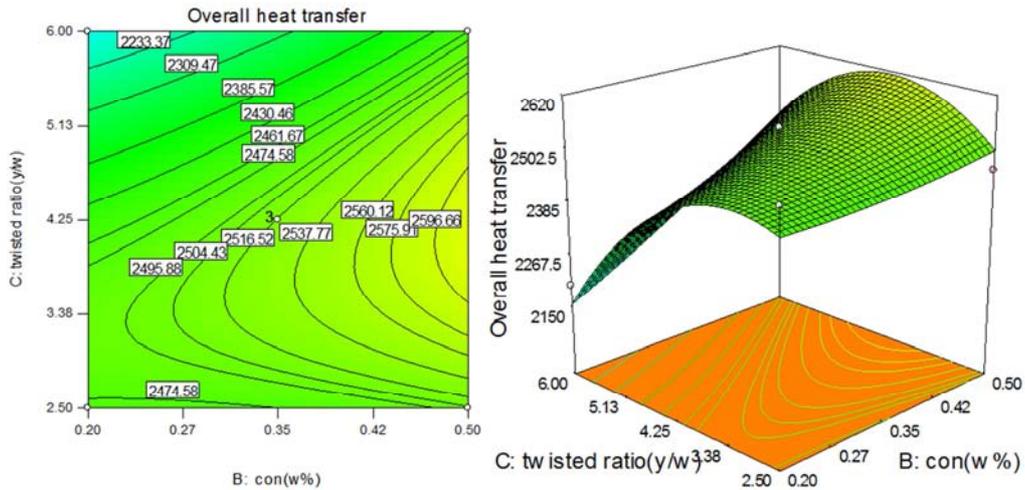


Figure 7. Response surface plots for the effect of the concentration(w%) and twisted ratio(y/w) on the overall heat transfer coefficients.

Figures 8 and 9 show the optimization plot with a desirability of 0.937 generated by RSM. It shows that the optimum value of the overall heat transfer coefficients is 2732.59 (w/m2.k) when the Reynolds number u_t is 19999.42, concentration (0.5%w) and twisted ratio (y/w) 5.87.

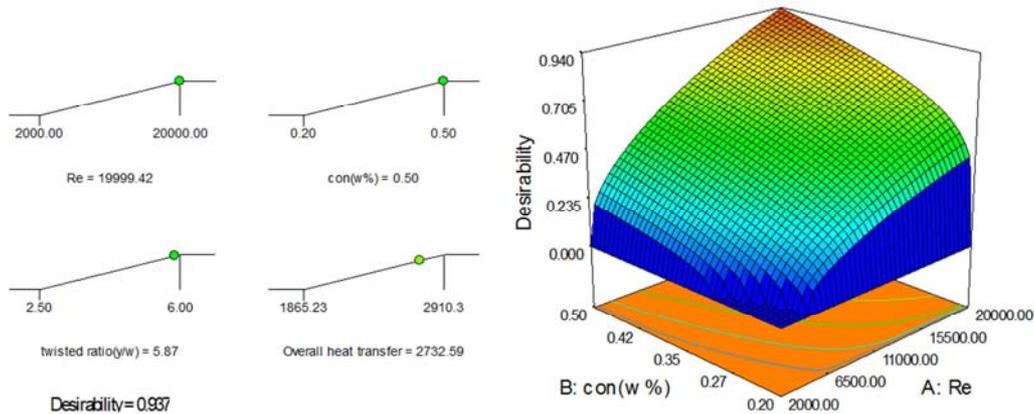


Figure 8. Optimization plot for double pipe heat exchanger.

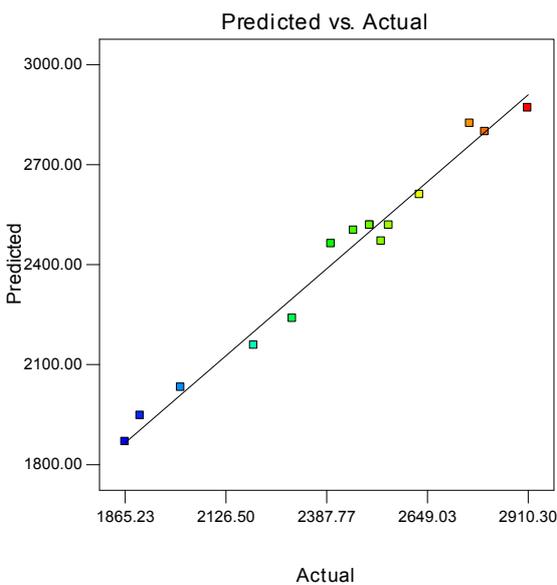


Figure 9. Comparison of predicted and experimental values.

The confirmation tests are conducted and the errors are tabulated in the figure 9. The findings show that the errors between the experimental and predicted values are less than 3%. It denotes that the predicted model is efficient.

5. Conclusion

In this paper, the experimental results showed the overall heat transfer coefficients of the double pipe heat exchanger and the statistical analysis results demonstrated that the effects of various operating parameters on the overall heat transfer coefficients. Empirical relation for overall heat transfer coefficients was developed to correlate dominant input parameters like Reynolds number, twisted ratio (y/w) and concentration of SiO₂ nanofluid of coolant using Response Surface Methodology. The influence of input parameters on the performance of double pipe heat exchanger was analyzed based on the developed relation by RSM. The predicted value of RSM are very closer to the experimental results and it has reduced the number of experiments, because RSM provides useful interaction between different

variables of the system. In the desirability function approach, the value of desirability was 0.937 for the RSM model very close to The predicted RSM model is found to be capable of predictive overall heat transfer coefficients of double pipe heat exchanger's showed a better accuracy and capability of generalization with the design of experiments.

References

- [1] Choi, S. U. S. "Enhancing thermal conductivity of fluids with nanoparticles", In: D. A. Siginer and H. P. Wang (Eds), *Developments and Applications of Non-Newtonian Flows*, ASME FED, 231/MD, 66, pp. 99- 105, 1995.
- [2] Jaafar Albadr, Satinder Tayal, Mushtaq Alasadi. "Heat transfer through heat exchanger using Al₂O₃ nanofluids at different concentrations". *Case Studies in Thermal Engineering* 1 (2013) 38–44.
- [3] D. Madhesh, R. Parameshwaran, S. Kalaiselvam. "Experimental investigation on convective heat transfer and rheological characteristics of Cu–TiO₂ hybrid nanofluids". *Experimental Thermal and Fluid Science* 52 (2014) 104–115.
- [4] Mostafa Keshavarz Moraveji, Reza Mohammadi Ardehali. "CFD modeling (comparing single and two-phase approaches) on thermal performance of Al₂O₃/water nanofluid in mini-channel heat sink". *International Communications in Heat and Mass Transfer* 44 (2013) 157–164.
- [5] M. A. Ahmed, M. Z. Yusoff, K. C. N, N. H. Shuaib. "The effect softway-wall phase shift on thermal-hydraulic performance of Al₂O₃–water nanofluid flow in sinusoidal-wavy channel *Studies in Thermal Engineering* 4(2014)153–165.
- [6] W. H. Azmi, K. V. Sharma, P. K. Sarma c, Rizalman Mamat, Shahrani Anuar. "Comparison of convective heat transfer coefficient and friction factor of TiO₂ nanofluid flow in a tube with twisted tape inserts". *International Journal of Thermal Sciences* 81 (2014) 84-93.
- [7] Ali Celen, Nurullah Kayaci, Alican Çebi, Hakan Demir, Ahmet Selim Dalkılıç, Somchai Wongwises. "Numerical investigation for the calculation of TiO₂–water nanofluids' pressure drop in plain and enhanced pipes". *International Communications in Heat and Mass Transfer* 53 (2014) 98–108.
- [8] M. Chandra Sekhara Reddy, Veeredhi Vasudeva Rao. "Experimental investigation of heat transfer coefficient and friction factor of ethylene glycol water based TiO₂ nanofluid in double pipe heat exchanger with and without helical coil inserts", *International Communications in Heat and Mass Transfer* 50, (2014)68–76.
- [9] K. V. Sharma, L. Syam Sundar, P. K. Sarma, "Estimation of heat transfer coefficient and friction factor in the transition flow with low volume concentration of Al₂O₃ nanofluid flowing in a circular tube and with twisted tape insert", *Int. Commun. Heat Mass Transf.*, 36 (2009), pp. 503–507
- [10] L. Syam Sundar, K. V. Sharma "Turbulent heat transfer and friction factor of Al₂O₃ nanofluid in circular tube with twisted tape inserts", *Int. J. Heat Mass Transf.*, 53 (2010), pp. 1409–1416
- [11] G. Pathipakka, P. Sivashanmugam "Heat transfer behaviour of nanofluids in a uniformly heated circular tube fitted with helical inserts in laminar flow", *Superlattices Microstruct.*, 47 (2010), pp. 349–360.
- [12] K. Wongcharee, S. Eiamsa-ard "Enhancement of heat transfer using CuO/water nanofluid and twisted tape with alternate axis", *Int. Commun. Heat Mass Transf.*, 38 (2011), pp. 742–748.
- [13] K. Wongcharee, S. Eiamsa-ard "Heat transfer enhancement by using CuO/water nanofluid in corrugated tube equipped with twisted tape", *Int. Commun. Heat Mass Transf.*, 39 (2012), pp. 251–257.
- [14] S. Eiamsa-ard, K. Wongcharee "Single-phase heat transfer of CuO/water nanofluids in micro-fin tube equipped with dual twisted-tapes", *Int. Commun. Heat Mass Transf.*, 39 (2012), pp. 1453–1459.
- [15] S. Suresh, K. P. Venkitaraj, P. Selvakumar "Comparative study on thermal performance of helical screw tape inserts in laminar flow using Al₂O₃/water and CuO/water nanofluids", *Superlattices Microstruct.*, 49 (2011), pp. 608–622.
- [16] S. Suresh, K. P. Venkitaraj, P. Selvakumar, M. Chandrasekar "A comparison of thermal characteristics of Al₂O₃/water and CuO/water nanofluids in transition flow through a straight circular duct fitted with helical screw tape inserts", *Exp. Therm. Fluid Sci.*, 39 (2012), pp. 37–44.
- [17] V. T. Perarasu, M. Arivazhagan, P. Sivashanmugam "Heat transfer of TiO₂/water nanofluid in a coiled agitated vessel with propeller", *J. Hydrodyn. Ser. B*, 24 (2012), pp. 942–950.
- [18] P. K. Nagarajan, YagnaMukkamala, P. Sivashanmugam, Studies on heat transfer and friction factor characteristics of turbulent flow through a micro finned tube fitted with left-right inserts, *Appl. Therm. Eng.* 30 (2010) 1666e1672.