

Semi-analytical and numerical solution of regularized Burdet equations to predict the motion of an artificial satellite

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Abstract: In this paper, literal analytical solution in power series forms which is one of the semi-analytical solution, are developed for the regularized Burdet equations to estimate the motion of an artificial satellite under the influence of J_2 -Earth's gravitational field. Also a numerical solution of the regularized Burdet equations is applied using eighth order Dormand-Prince Rung-Kutta method. Comparison between the power series solution and the numerical solution applied to high eccentric frozen satellite orbit is also given and showed excellent agreement.

Keywords: Astrodynamics, Satellite Orbit Determination, Power Series, Numerical integration

1. Introduction

It is well known that the solutions of the Classical Newtonian Equations of motion are unstable and these equations are not suitable for long-term integrations. Many transformations have emerged in the literature in the recent past to stabilize the equations of motion either to reduce the accumulation of local numerical errors or allowing of using a larger integration step size, in the transformed space, or both ([9], [1] and [6]). One of such transformation, known as the Sperling/Burdet Equations, is due to [17] and [3] who regularized the non-linear Kepler motion and reduced it to linear differential equations of a harmonic oscillator of constant frequency. Reference [5] outlined the differential equations and the initial value problem together with the transformation to rectangular coordinates and classical elements. The Burdet's variables can be adopted for the computation of elliptic, parabolic and hyperbolic motion ([13]). References [12], [1] and [6] applied this method numerically to predict a satellite motion.

In spite of their advantages in many cases, analytical methods do not always provide high-accuracy solutions to orbital problems, as required. Both analytical and semi-analytical methods use an analytical transformation to produce mean, slowly varying differential equations ([2], [14], [15] and [16]). However, analytical solutions, though difficult to obtain for complex force models and limited to relatively simple models, represent a manifold of solutions

for a large domain of initial conditions and parameters and find indispensable application to mission planning and qualitative analysis. Otherwise power series solution (which of course assumed to be convergent) can serve as the analytical representation of its solution. Moreover, it is worth noting that the power series is one of the most powerful methods of mathematical analysis when the problems are to be studied on computers. In fact, most computers often use series in the calculations of the majority of the elementary functions.

For the numerical solution, We have the Dormand-Prince method, which is an explicit method for solving ordinary differential equations ([4]). The method is a member of the Runge-Kutta family of ODE solvers and its eighth order uses 12 function evaluations with $err = O(h^8)$ where h is the step size ([8] and [10]).

In this paper, we construct a recurrent power series solution for the Sperling-Burdet perturbed differential equations of motion depending on Taylor series expansion to get the classical elements of the satellite at any time. We apply the eighth order Dormand-Prince method to these equations to get the numerical solution and compare this solution with the power series solution.

2. Formulation of the Problem

Generally, the equations of motion of an artificial satellite are given generally as

$$\ddot{\vec{x}} + \frac{\mu}{r^3} \vec{x} = \vec{T} \quad (1)$$

where \vec{x} is the relative position vector, $r = |\vec{x}|$, μ is the Earth's gravitational constant, \vec{T} is the all perturbing forces, which equals to $\left(-\frac{\partial V}{\partial \vec{x}} + \vec{P}^* \right)$, where \vec{P}^* is the resultant of all non-conservative perturbing forces, and V is the perturbed time-independent potential, which can be expressed as

$$V = \mu \sum_{i=2}^{\infty} R_{\oplus}^i J_i (1/r)^{i+1} L_i(x_3/r)$$

where R_{\oplus} is the Earth's equatorial radius, J_i is the non-dimensional coefficient of the Earth's potential and L_i is the Legendre polynomial of order i ([11]).

In our case the only force acting on an artificial satellite is that due to the Earth's oblateness, so we have

$$\vec{P}^* = 0, \quad (2.1)$$

$$V = \frac{3}{2} q_2 x_3^2 r^{-5} - \frac{1}{2} q_2 r^{-5} \quad (2.2)$$

where $q_2 = \mu R_{\oplus}^2 J_2$ and $r = \sqrt{x_1^2 + x_2^2 + x_3^2}$.

Eq. (1) are the basic classical equations of motion of artificial satellites and the corresponding perturbed equations of motion with the independent variable (true anomaly) in terms of the Burdet's parameters ([5] and [12]) are

$$\ddot{\xi} + \xi = \mu^{-1} p^{-1} u^{-3} (\bar{T} - \langle \bar{T}, \xi \rangle \bar{\xi}) - \frac{1}{2} p^{-1} p' \xi', \quad (3.1)$$

$$u'' + u = (p)^{-1} - (\mu p u^2)^{-1} \langle \bar{T}, \xi \rangle - (2p)^{-1} p' u', \quad (3.2)$$

$$p' = 2 (\mu u^3)^{-1} \langle \bar{T}, \xi' \rangle, \quad (3.3)$$

$$t' = (\mu p)^{-1/2} u^{-2}, \quad (3.4)$$

where

$$u = 1/r,$$

$$\bar{\xi} = \vec{x}/r = u \vec{x};$$

$$p = \left(\frac{r^2}{\mu} \right) \left(\dot{\vec{x}} \cdot \dot{\vec{x}} - \dot{r}^2 \right),$$

$$\text{and} \quad \bar{T} = -\frac{\partial V}{\partial \vec{x}} + \vec{P}^*;$$

Hence $\langle \vec{a}, \vec{b} \rangle$ is used to denote the scalar product of two vectors \vec{a} and \vec{b} . Denoting differentiation with respect to the new time f (true anomaly) by a prime ($'$), since

the independent variable is changed from time (t) to new time (f) according to

$$\frac{df}{dt} = \frac{\sqrt{\mu p}}{r^2},$$

([3] and [12]).

After transform Eqs (3) into ten first order differential equations, we get

$$g'_1 = g_4, \quad (4.1)$$

$$g'_2 = g_5, \quad (4.2)$$

$$g'_3 = g_6, \quad (4.3)$$

$$g'_4 = -g_1 + (\mu g_9)^{-1} g_7^{-3} \{T_1 - g_1 [T_1 g_1 + T_2 g_2 + T_3 g_3]\} - 0.5 g_9^{-1} g'_9 g_4, \quad (4.4)$$

$$g'_5 = -g_2 + (\mu g_9)^{-1} g_7^{-3} \{T_2 - g_2 [T_1 g_1 + T_2 g_2 + T_3 g_3]\} - 0.5 g_9^{-1} g'_9 g_5, \quad (4.5)$$

$$g'_6 = -g_3 + (\mu g_9)^{-1} g_7^{-3} \{T_3 - g_3 [T_1 g_1 + T_2 g_2 + T_3 g_3]\} - 0.5 g_9^{-1} g'_9 g_6, \quad (4.6)$$

$$g'_7 = g_8, \quad (4.7)$$

$$g'_8 = -g_7 + g_9^{-1} - (\mu g_9)^{-1} g_7^{-2} \{T_1 g_1 + T_2 g_2 + T_3 g_3\} - 0.5 g_9^{-1} g'_9 g_8, \quad (4.8)$$

$$g'_9 = 2 (\mu g_7)^{-1} \{T_1 g_4 + T_2 g_5 + T_3 g_6\}, \quad (4.9)$$

$$g'_{10} = g_7^{-2} (\mu g_9)^{-1/2}. \quad (4.10)$$

where

$$g_i = \xi_i = u x_i, \quad g_{i+3} = \xi'_i, \quad i = 1, 2, 3;$$

$$g_7 = u,$$

$$g_8 = u',$$

$$g_9 = p^*,$$

$$\text{and} \quad g_{10} = t.$$

and we have from Eq. (2.2)

$$T_1 = \frac{3}{2} \mu J_2 R_{\oplus}^2 g_1 g_7^4 (5 g_3^2 - 1), \quad (5.1)$$

$$T_2 = \frac{3}{2} \mu J_2 R_{\oplus}^2 g_2 g_7^4 (5 g_3^2 - 1); \quad (5.2)$$

$$T_3 = \frac{3}{2} \mu J_2 R_{\oplus}^2 g_3 g_7^4 (5 g_3^2 - 3). \quad (5.3)$$

3. Recurrent Power Series Solution

In this section, recurrent power series solution of Eqs.(3) will be constructed as follow.

3.1. Auxiliary dependent variables

Let us define the following auxiliary dependent functions, which transform the system of differential equations of motion in a new system of differential equations where all denominators have been removed, as well as all the powers of g_i .

$$\begin{aligned} a_1 &= g_7 g_7; & a_2 &= a_1 a_1; \\ a_3 &= g_3 g_3; & Q &= \frac{3}{2} \mu J_2 R_\oplus^2; \\ f_i &= g_i a_2 \quad i=1,2,3; & f_{i3} &= f_i a_3 \quad i=1,2,3; \\ t_1 &= 5 Q f_{13} - Q f_1; & t_2 &= 5 Q f_{23} - Q f_2; \\ t_3 &= 5 Q f_{33} - 3 Q f_3; \\ b_6 &= t_1 g_1 + t_2 g_2 + t_3 g_3; \\ y_i &= b_6 g_i \quad i=1,2,3; \\ y_{ii} &= t_i - y_i \quad i=1,2,3; \\ g_{11} &= g_7^{-1} = 1/g_7; & g_{12} &= g_{11} g_{11}; \\ g_{13} &= g_{11} g_{12}; & g_{14} &= g_9^{-1} = 1/g_9; \\ g_{15} &= g_9^{-1/2} = 1/\sqrt{g_9}; & g_{16} &= g_{15} g_{12}; \\ b_4 &= t_1 g_4 + t_2 g_5 + t_3 g_6; & b_5 &= g_{13} b_4; \\ g_{17} &= g_{13} g_{14}; & g_{18} &= b_5 g_{14}; \\ g_{7i} &= g_{17} y_{ii} \quad i=1,2,3; \\ g_{8i} &= g_{18} g_i \quad i=4,5,6; \\ \text{and} \end{aligned}$$

$$g_{19} = g_{14} g_{12}; \quad g_{20} = g_{19} b_6; \quad g_{21} = g_8 g_{18};$$

Using the previous substitutions into Eqs.(4), we get the following first order differential set in ten unknowns

$$g'_1 = g_4, \quad (6.1)$$

$$g'_2 = g_5, \quad (6.2)$$

$$g'_3 = g_6, \quad (6.3)$$

$$g'_4 = -g_1 + \frac{1}{\mu} g_{71} - \frac{1}{\mu} g_{84}; \quad (6.4)$$

$$g'_5 = -g_2 + \frac{1}{\mu} g_{72} - \frac{1}{\mu} g_{85}; \quad (6.5)$$

$$g'_6 = -g_3 + \frac{1}{\mu} g_{73} - \frac{1}{\mu} g_{86}; \quad (6.6)$$

$$g'_7 = g_8; \quad (6.7)$$

$$g'_8 = -g_7 + g_{14} - \frac{1}{\mu} g_{20} - \frac{1}{\mu} g_{21}; \quad (6.8)$$

$$g'_9 = \frac{2}{\mu} b_5; \quad (6.9)$$

$$g'_{10} = \frac{1}{\sqrt{\mu}} g_{16}. \quad (6.10)$$

3.2. Power series manipulations

Let us define the ten Taylor expansions as follows

$$h_i = \sum_{n=0}^{\infty} H_i^{(n)} f^n; \quad i=1,2,\dots,10 \quad (7)$$

and

$$h'_i = \sum_{n=0}^{\infty} (n+1) H_i^{(n+1)} f^n; \quad (8)$$

where we have used small letters (h) for the unknown variables and capital letters (H) for the coefficients in their Taylor series expansion.

Now, let us define a and b as two convergent power series such that

$$a = \sum_{i=0}^{\infty} A^{(i)} s^i,$$

$$b = \sum_{i=0}^{\infty} B^{(i)} s^i.$$

Then, we have (Gradshteyn and Ryzhik, 2007)

- Division of power series

$$\frac{b}{a} = \frac{1}{A^{(0)}} \sum_{k=1}^{\infty} C^{(k)} s^k$$

where

$$C^{(0)} = B^{(0)}, \quad C^{(k)} = B^{(k)} - \frac{1}{A^{(0)}} \sum_{i=1}^k C^{(k-i)} A^{(i)} \quad k=1,2,\dots$$

- Power series raised to powers

$$a^n = \left(\sum_{i=0}^{\infty} A^{(i)} s^i \right)^n = \sum_{i=0}^{\infty} P^{(i)} s^i$$

where

$$P^{(0)} = (A^{(0)})^n, \quad P^{(k)} = \frac{1}{k A^{(0)}} \sum_{i=1}^k (in - k + i) P^{(k-i)} A^{(i)} \quad \forall k \geq 1$$

- Multiplication of power series

$$c = a b = \sum_{n=0}^{\infty} C^{(n)} s^n,$$

where

$$C^{(n)} = \sum_{i=0}^n A^{(i)} B^{(n-i)}.$$

Substituting Eqs.(7) and (8) into Eqs.(6), and using the above rules for the power series, and equating coefficients of equal powers of f in both sides of each of the resulting equations, then we get the coefficients of the following recurrence formulae

$$n G_1^{(n+1)} = G_4^{(n)}; \quad (9.1)$$

$$n G_2^{(n+1)} = G_5^{(n)}; \quad (9.2)$$

$$n G_3^{(n+1)} = G_6^{(n)}; \quad (9.3)$$

$$n G_4^{(n+1)} = -G_1^{(n)} + \frac{1}{\mu} G_{71}^{(n)} - \frac{1}{\mu} G_{84}^{(n)}; \quad (9.4)$$

$$n G_5^{(n+1)} = -G_2^{(n)} + \frac{1}{\mu} G_{72}^{(n)} - \frac{1}{\mu} G_{85}^{(n)}; \quad (9.5)$$

$$n G_6^{(n+1)} = -G_3^{(n)} + \frac{1}{\mu} G_{73}^{(n)} - \frac{1}{\mu} G_{86}^{(n)}; \quad (9.6)$$

$$n G_7^{(n+1)} = G_8^{(n)}; \quad (9.7)$$

$$n G_8^{(n+1)} = -G_7^{(n)} + G_{14}^{(n)} - \frac{1}{\mu} G_{20}^{(n)} - \frac{1}{\mu} G_{21}^{(n)}; \quad (9.8)$$

$$n G_9^{(n+1)} = \frac{2}{\mu} B_5^{(n)}; \quad (9.9)$$

$$n G_{10}^{(n+1)} = \frac{1}{\sqrt{\mu}} G_{16}^{(n)}. \quad (9.10)$$

then we can compute the coefficients (capital letters) to get small letters which are the unknown variables (g's).

4. Computational Developments

In this section, the computational developments of the formulation of section 3 for power series will be considered. For the eighth order Dormand-Prince method will be applied on the first differential Eqs (4).

4.1. Computation Of The Initial Values:

Knowing the classical elements $\{a, e, M, i, \omega, \Omega\}$ at some time t_0 (corresponding to f_0), we can get the position vector \vec{x}_0 and the velocity vector $\dot{\vec{x}}_0$ at the same time t_0 ([18]), where a is a semi major axis, e is an eccentricity, M is a mean anomaly, i is an inclination, ω is an argument of perigee and Ω is a longitude of the ascending node.

Now we can compute

$$r_0 = \sqrt{x_{01}^2 + x_{02}^2 + x_{03}^2}, \text{ and } \dot{r}_0 = (1/r_0)(x_{01}\dot{x}_{01} + x_{02}\dot{x}_{02} + x_{03}\dot{x}_{03}).$$

and we can get g's as follows

$$g_{0i} = x_{0i} / r_0,$$

$$g_{0,i+3} = (r_0 \dot{x}_{0,i} - \dot{r}_0 x_{0,i}) / \sqrt{\mu g_{09}}, \quad i = 1, 2, 3;$$

$$g_{07} = 1/r_0,$$

$$g_{08} = -\dot{r}_0 / \sqrt{\mu g_{09}},$$

$$g_{09} = (r_0^2 / \mu)(\dot{x}_{01}^2 + \dot{x}_{02}^2 + \dot{x}_{03}^2 - \dot{r}_0^2),$$

$$\text{and } g_{10} = t_0.$$

Vice versa, the position and velocity are obtained from the g's as the following relations

$$x_i = g_i / g_7, \text{ and } \dot{x}_i = (g_7 g_{i+3} - g_8 g_i) \sqrt{\mu g_9}.$$

Finally, we get the classical elements from the position vector \vec{x}_0 and the velocity vector $\dot{\vec{x}}_0$ at the same time t ([18]).

4.2. The accuracy check

The accuracy of the computed values of the g's variables at any new time f (corresponding to the time t) could be checked by the two following relation

$$g_1^2 + g_2^2 + g_3^2 = 1, \text{ and } g_1 g_1' + g_2 g_2' + g_3 g_3' = 0.$$

4.3. Utilization

When the true anomaly f is sufficiently large, we may (as usually done for all initial value problems) divide the interval f into some intervals into some intervals each of short length, e.g. the $(f - f_0)$ may be divided into $(r-1)$ intervals: $(f_1 - f_0), (f_2 - f_1), \dots, (f - f_q)$ such that $(f_h - f_{h-1}) \ll (f - f_0)$. Then solve the initial value problem for the first interval to find the solution at the value f_j . The solution at f_j could then be used as the initial condition for the second interval and so on. By this artifice one usually needs small number of the coefficients for the power series representation in each interval.

4.4. The step size Δf

The step size of the new time Δf could be computed from the corresponding step size Δt of the ordinary time as

$$\Delta f = \frac{\sqrt{\mu p}}{r^2} \Delta t.$$

4.5. Numerical test

In what follows the results of a comparison between the power series solution and the numerical integration of the first differential Equations 3 will be given. We use the following two line elements for MOLNIYA satellite which is highly eccentric frozen satellite orbit, as the initial conditions (www.spacetrack.com) at epoch 06 May 2014.

0 MOLNIYA 1-93

1 28163U 04005A 14115.76724197 .00000117 00000-0 00000+0 0 3266

2 28163 064.4633 083.5168 7312151 246.9027 252.2464 02.00655253 74609

We calculate the recurrent power series up to ten step (N=10), while the step size is $h = \frac{2\pi}{500}$, for 1000 cycle of

the satellite. The adopted physical constant are $R_\oplus = 1$ e.r. (earth radii), $\mu = 0.0055302632857476$ e.r.³/min², and the Earth's zonal harmonic coefficient J_2 equal 1.0826157×10^{-3} .

The results are illustrated graphically in the following figures, where the abscissa is the time. The accuracy check will be tabulated for every 100 cycle.

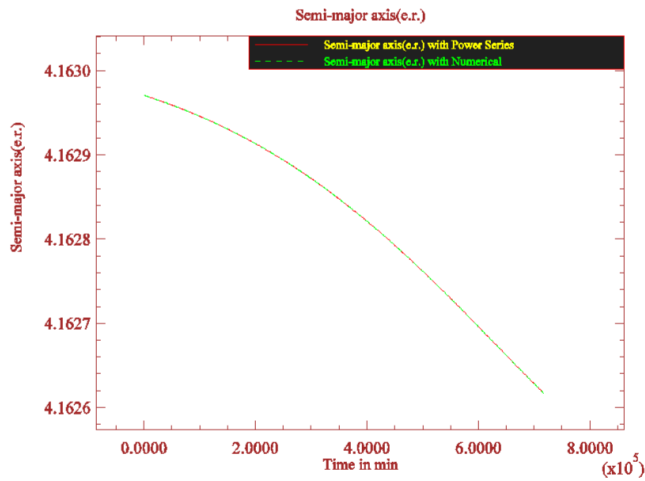


Fig. 1. Comparison between numerical and analytical solutions for the semi-major axis

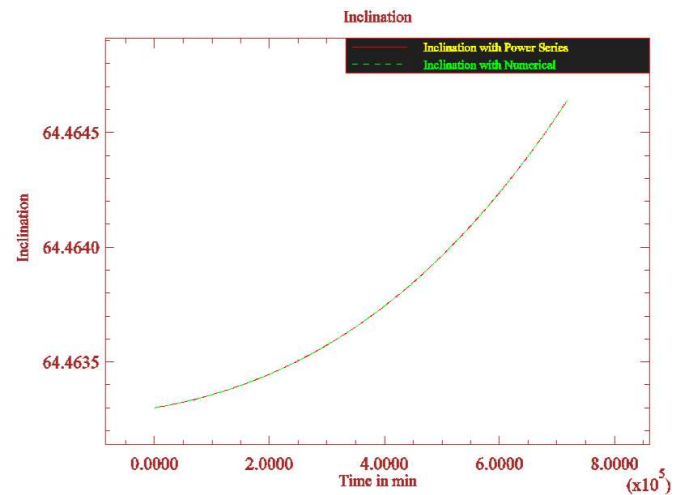


Fig. 4. Comparison between numerical and analytical solutions for the inclination

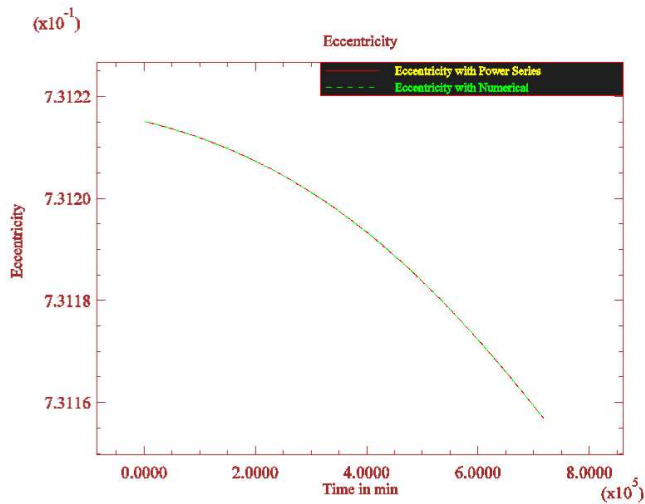


Fig. 2. Comparison between numerical and analytical solutions for the eccentricity

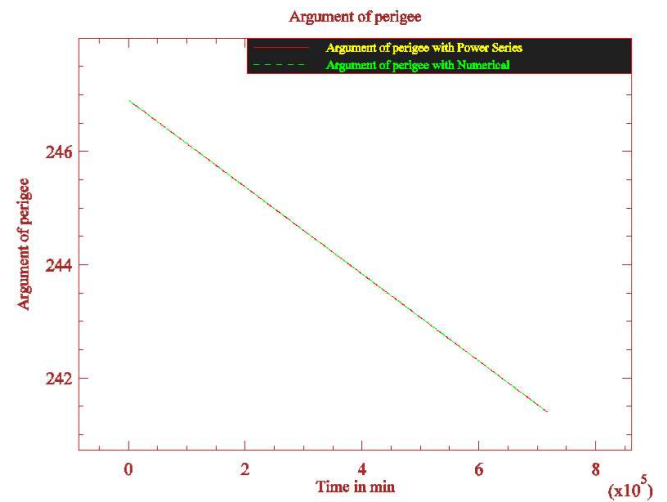


Fig. 5. Comparison between numerical and analytical solutions for the argument of perigee

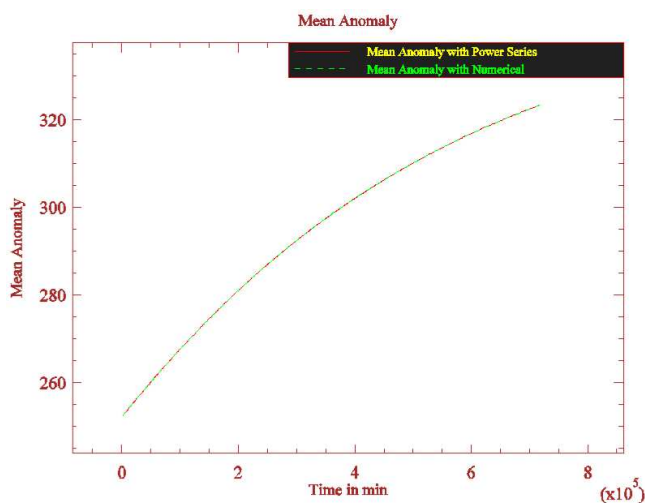


Fig. 3. Comparison between numerical and analytical solutions for the mean anomaly

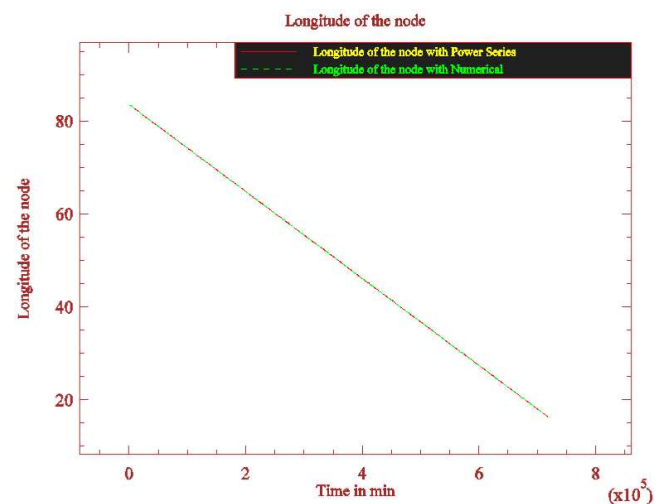


Fig. 6. Comparison between numerical and analytical solutions for the longitude of the ascending node

Table 1. The accuracy check

| No of Cycle | Time in minute | accuracy test for power series | | accuracy test for numerical integration | |
|-------------|----------------|----------------------------------|-------------------------|---|-------------------------|
| | | $g_1 g'_1 + g_2 g'_2 + g_3 g'_3$ | $g_1^2 + g_2^2 + g_3^2$ | $g_1 g'_1 + g_2 g'_2 + g_3 g'_3$ | $g_1^2 + g_2^2 + g_3^2$ |
| 1 | 1220.75679 | -5.117e-017 | 1.000e+000 | 2.682e-016 | 1.000e+000 |
| 100 | 71575.0487 | -4.946e-015 | 1.000e+000 | 4.384e-014 | 1.000e+000 |
| 200 | 143363.018 | -6.780e-015 | 1.000e+000 | 1.426e-013 | 1.000e+000 |
| 300 | 215148.873 | -4.260e-015 | 1.000e+000 | 3.069e-013 | 1.000e+000 |
| 400 | 286932.713 | -5.068e-015 | 1.000e+000 | 5.395e-013 | 1.000e+000 |
| 500 | 358714.681 | 9.418e-016 | 1.000e+000 | 8.280e-013 | 1.000e+000 |
| 600 | 430494.944 | 1.631e-015 | 1.000e+000 | 1.164e-012 | 1.000e+000 |
| 700 | 502273.681 | -5.379e-015 | 1.000e+000 | 1.539e-012 | 1.000e+000 |
| 800 | 574051.064 | -1.562e-014 | 1.000e+000 | 1.930e-012 | 1.000e+000 |
| 900 | 645827.259 | -2.238e-015 | 1.000e+000 | 2.335e-012 | 1.000e+000 |
| 1000 | 718320.164 | 1.019e-014 | 1.000e+000 | 2.727e-012 | 1.000e+000 |

5. Conclusion

From the figures we can conclude that, from the initial up to 500 mean solar days, there are obviously changes in the two elements (Ω , M), but the other elements (a , e , i) show lightly change, for the numerical integration and power series solutions. This expected because the only force affecting on the motion of artificial satellite is Earth's gravitational field (J_2), so the elements Ω , M behaviors are secular while the elements a , e , i have periodic treatment. But ω has very slightly change, as expect, because this satellite is frozen orbit (Molniya).

Also, the table shows the accuracy check for the two methods of solutions which one of them is always nearly to zero and the other is exact one, i.e., the predictions of the components of position and velocity (the elements) of the artificial satellite is very good.

The figures show that the comparison between the two methods, power series and numerical integration are identical. But the table of accuracy check show that the power series method is more accurate than the numerical integration. We can conclude the efficiency of the power series method.

To get more accurate prediction of the motion of the artificial satellite we will be taken into account the whole other forces affecting on the motion.

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